



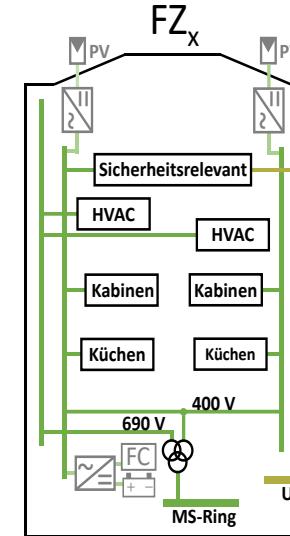
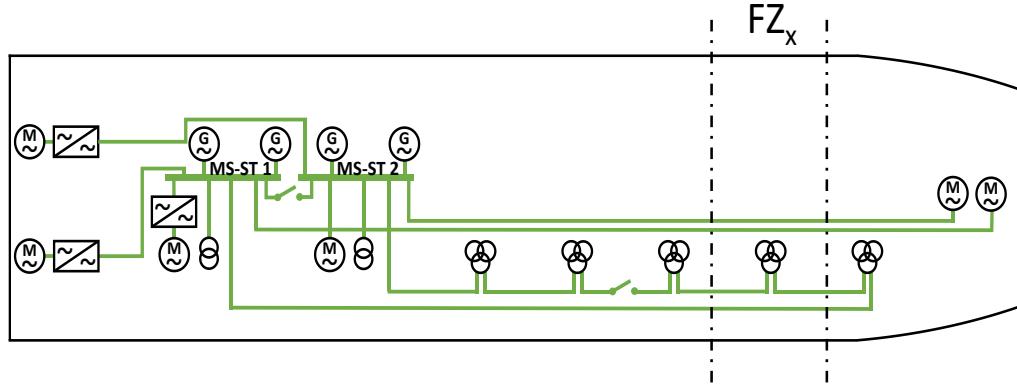
# Application of Impedance Measurement in Power Hardware-in-the-Loop Assisted Research

Konferenz Interessenverband Netzimpedanz – C. Klie – 15. Sep. 2022

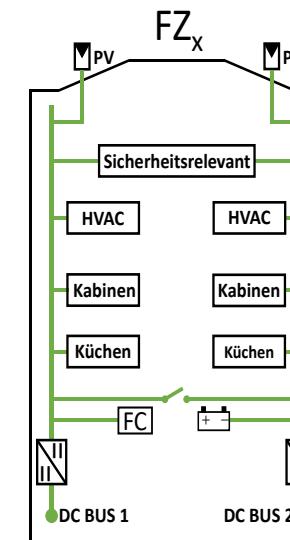
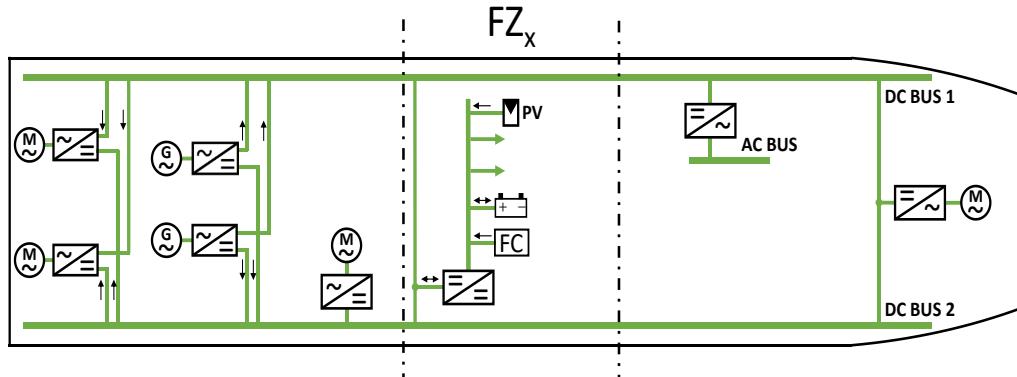
---

# SuSy: Sustainable DC Systems – Now and Then

## Traditional AC ship and firezone:



## Proposal for DC ship and firezone:



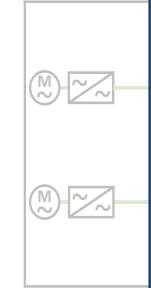
## General SuSy goals

- Overall reduction of cabling while maintaining secure operation
- Direct coupling of DC components to the grid

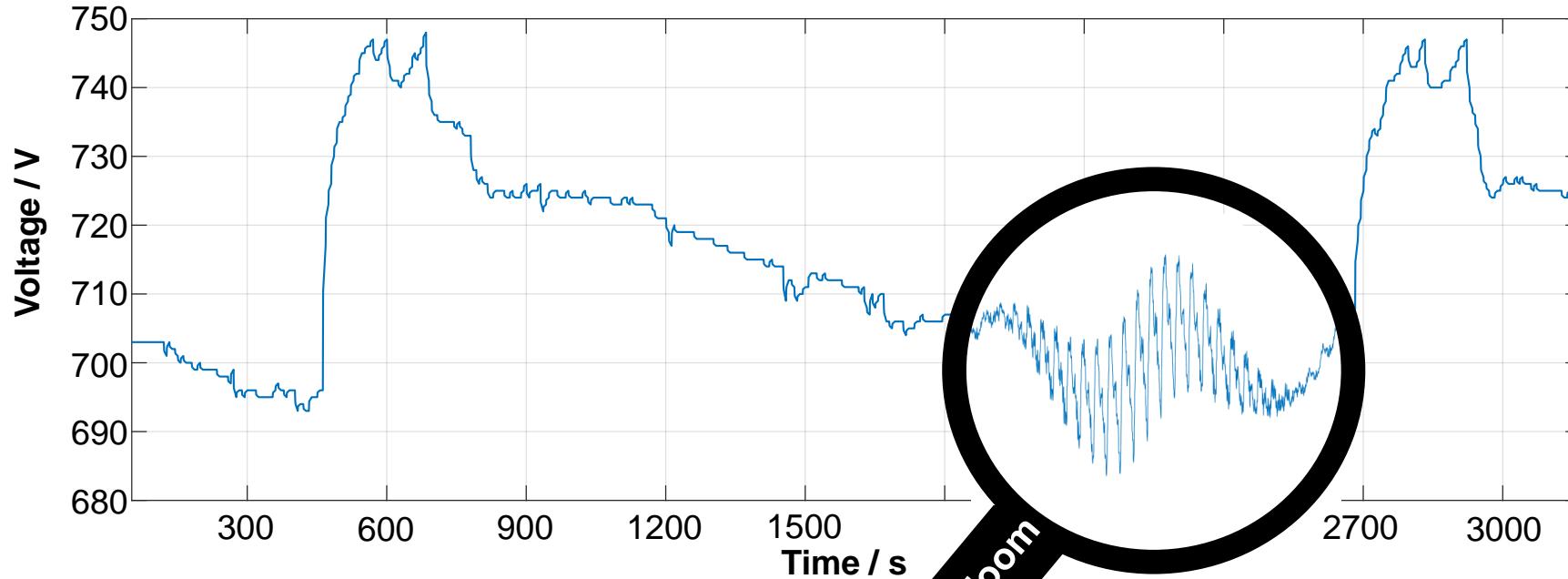
## TUHH goals in SuSy

- Investigation of equipment compatibility
- Investigation of control, stability, reliability and security

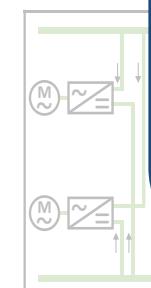
Traditional



## Measured DC-Bus voltage on ship type: „waterbus“ (DAMEN SHIPYARDS)

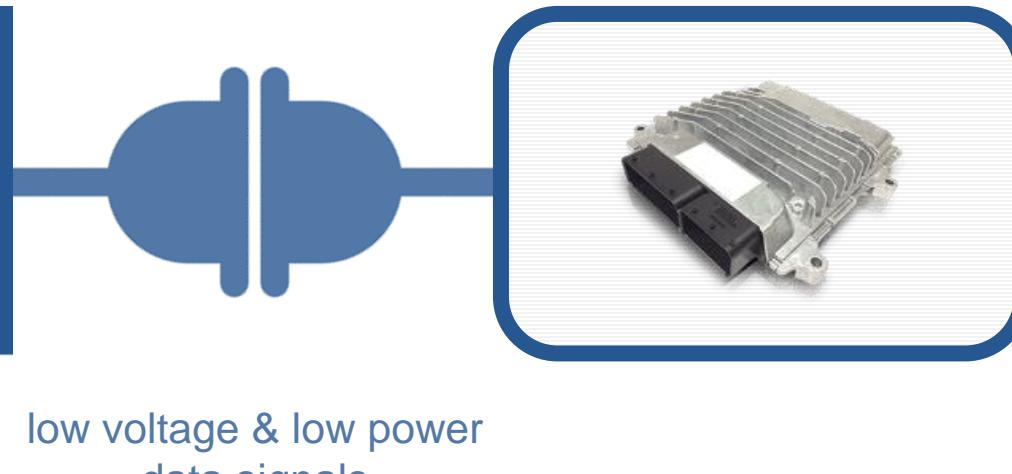
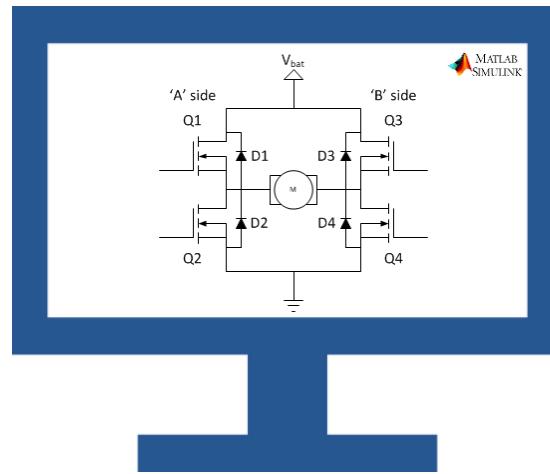


Proposed



# Hardware-in-the-Loop – The why and how

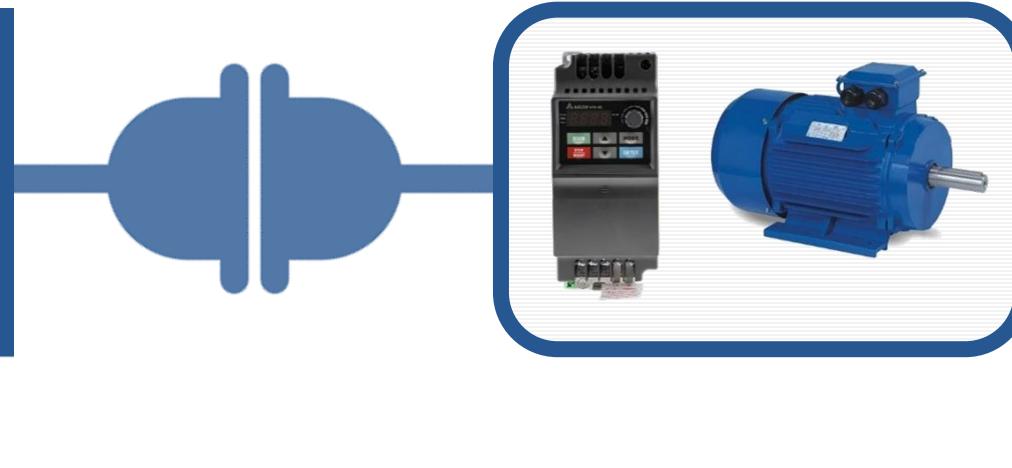
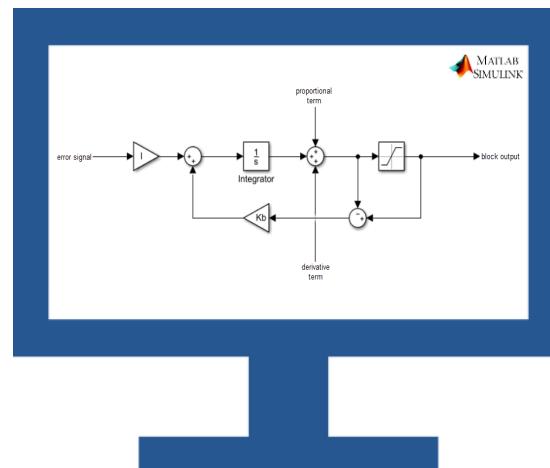
Realtime simulation  
of  
hardware components



Real controller

low voltage & low power  
data signals

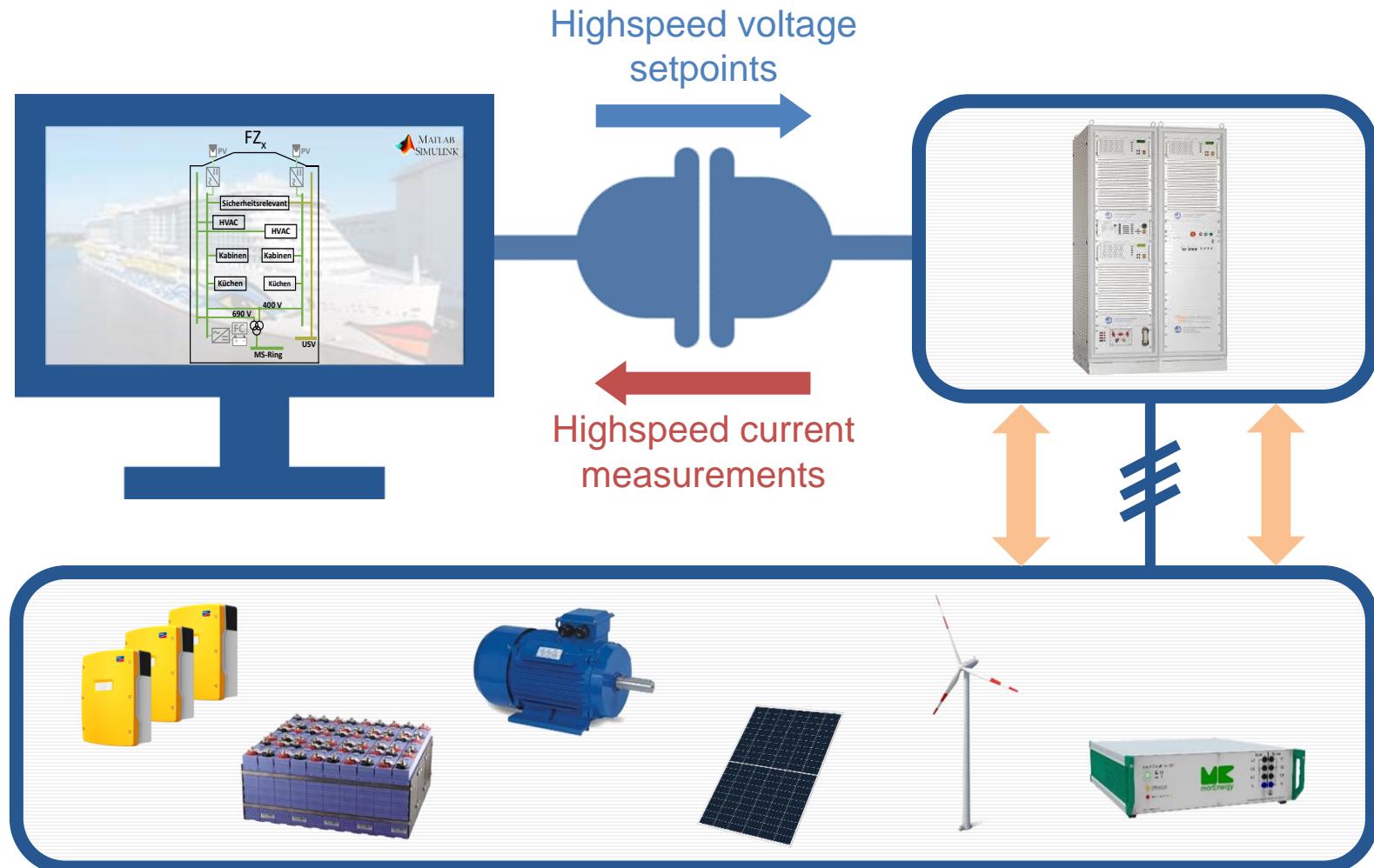
Realtime simulation  
of  
controller algorithms



Real hardware

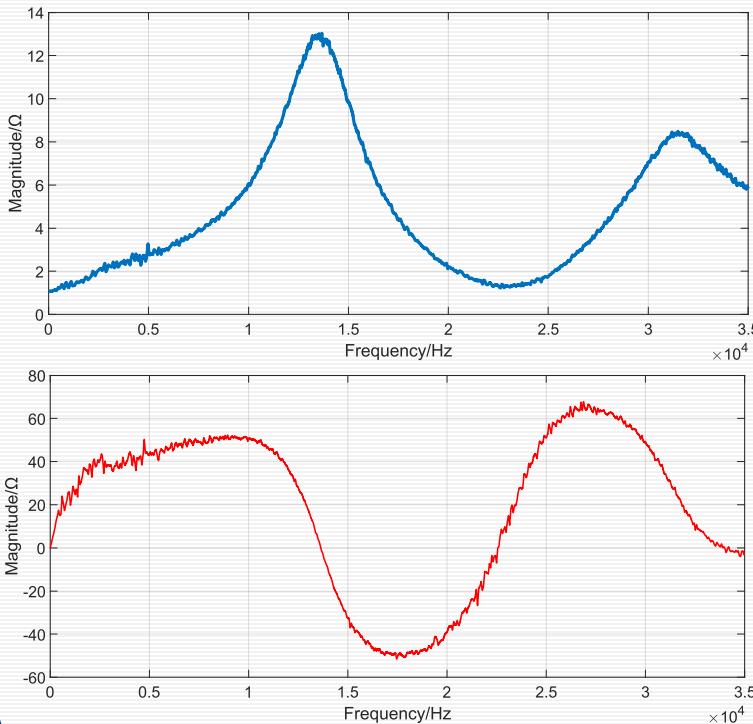
# Power Hardware-in-the-Loop – The next leap in HiL

Realtime simulation  
of  
large and complex  
grid structures

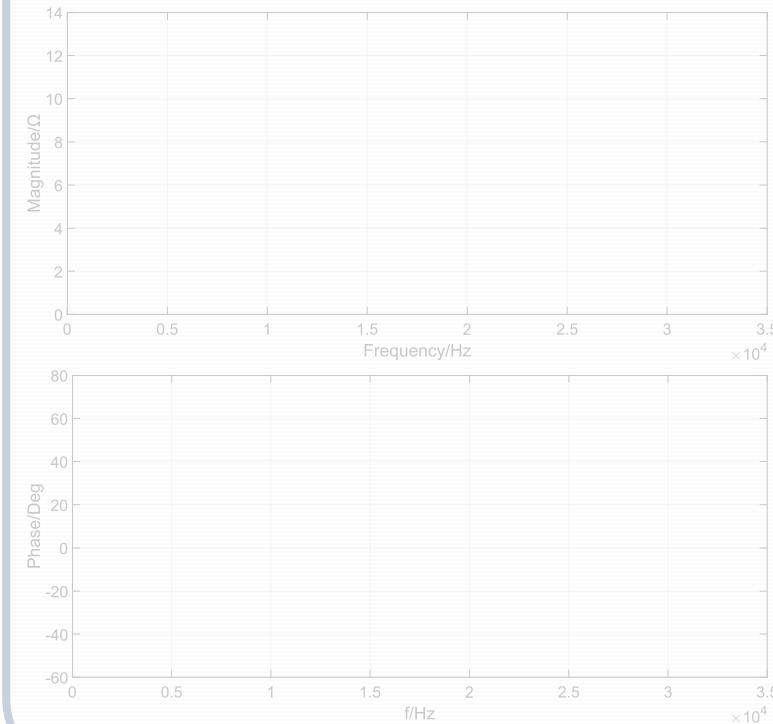


# PHiL Usecase: Impedance Replication of AIDAcosma

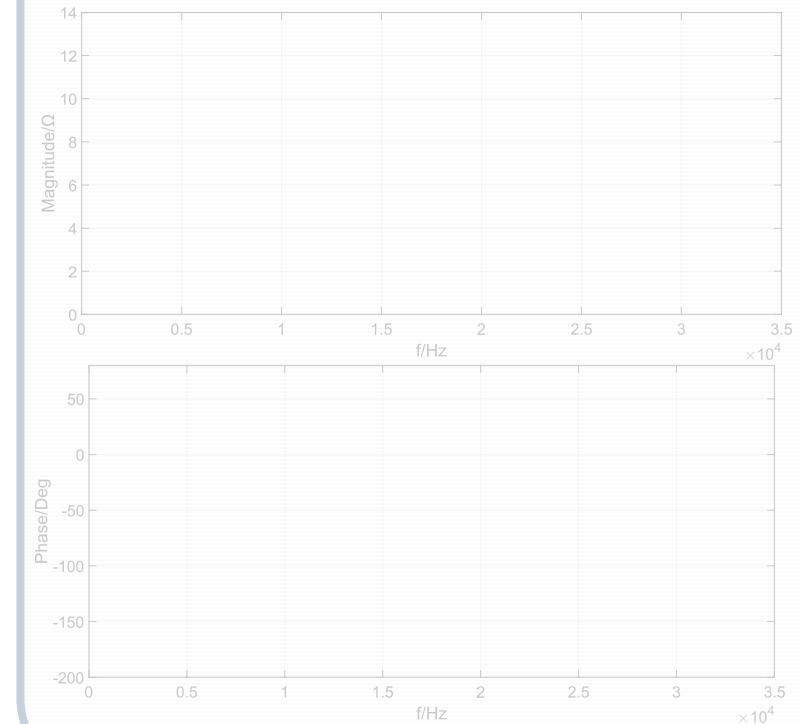
ONIS measurement  
on AIDAcosma



Simulink measurement of  
equivalent circuit on OP5707XG

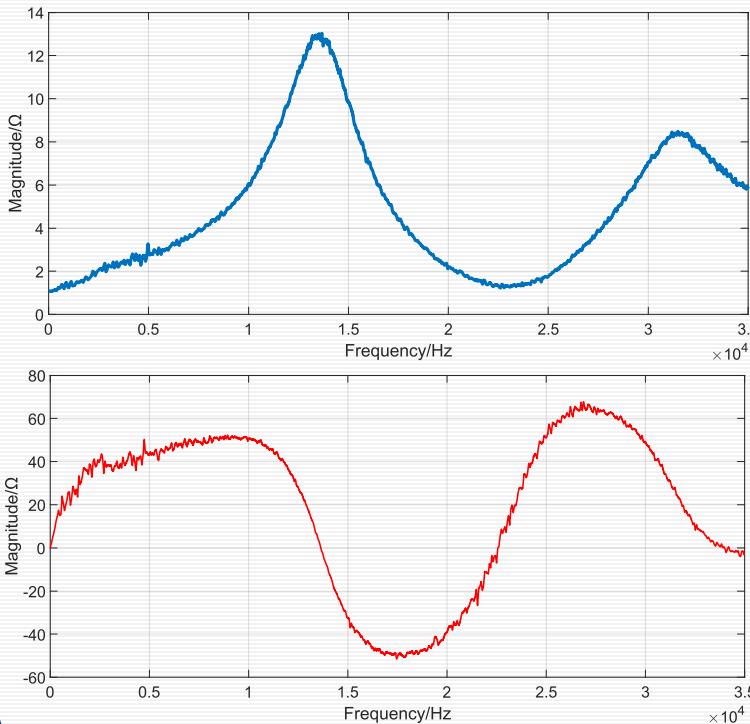


PHiL measurement  
with ONIS on Spitzenberger

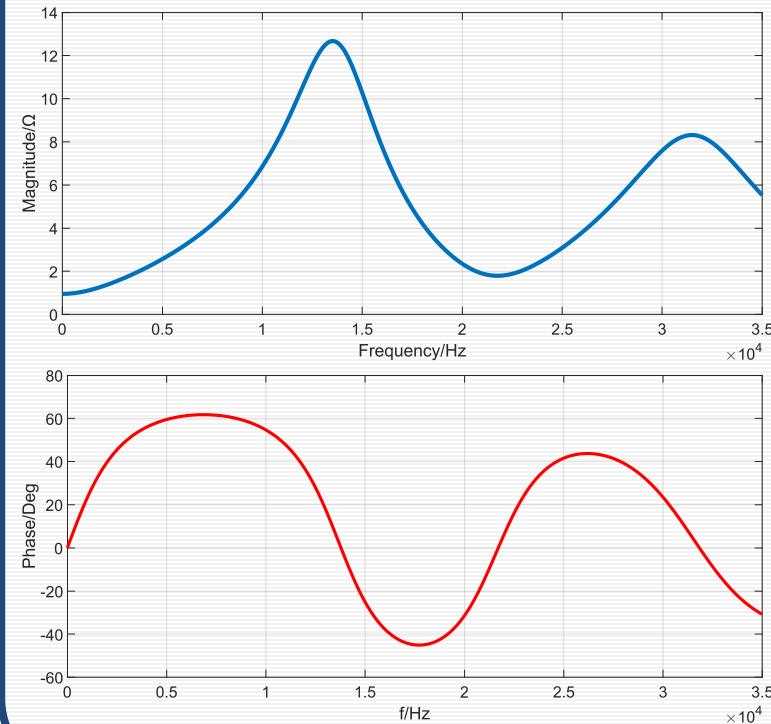


# PHiL Usecase: Impedance Replication of AIDAcosma

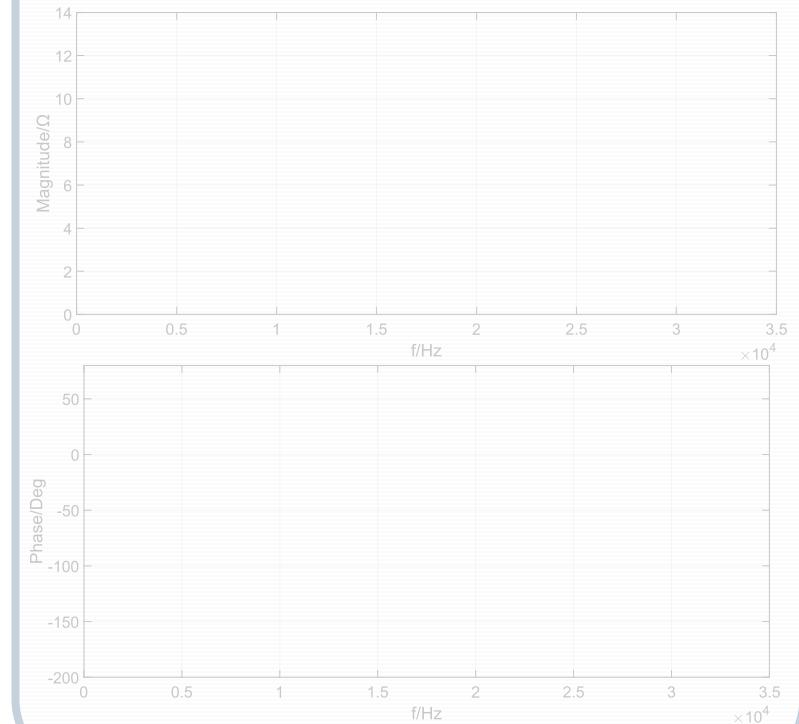
ONIS measurement  
on AIDAcosma



Simulink measurement of  
equivalent circuit on OP5707XG

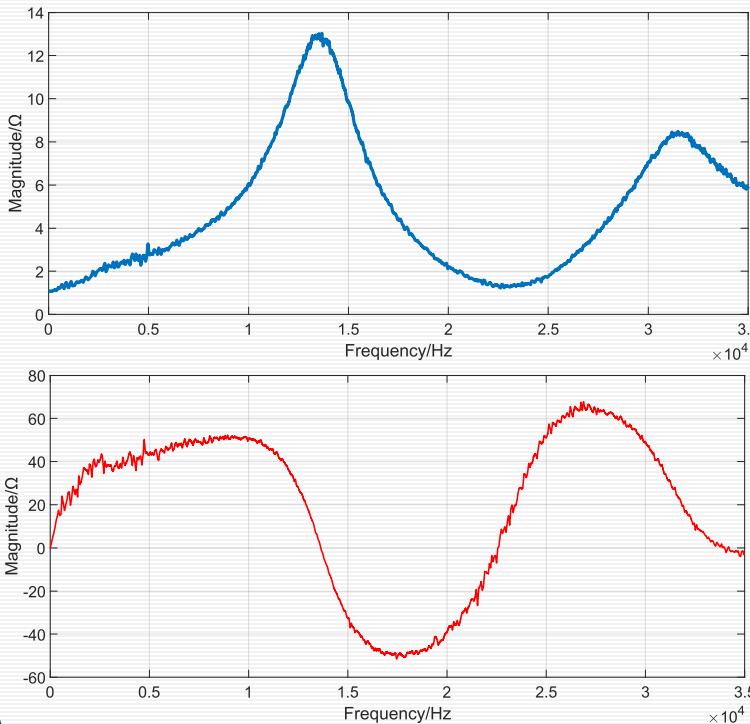


PHiL measurement  
with ONIS on Spitzenberger

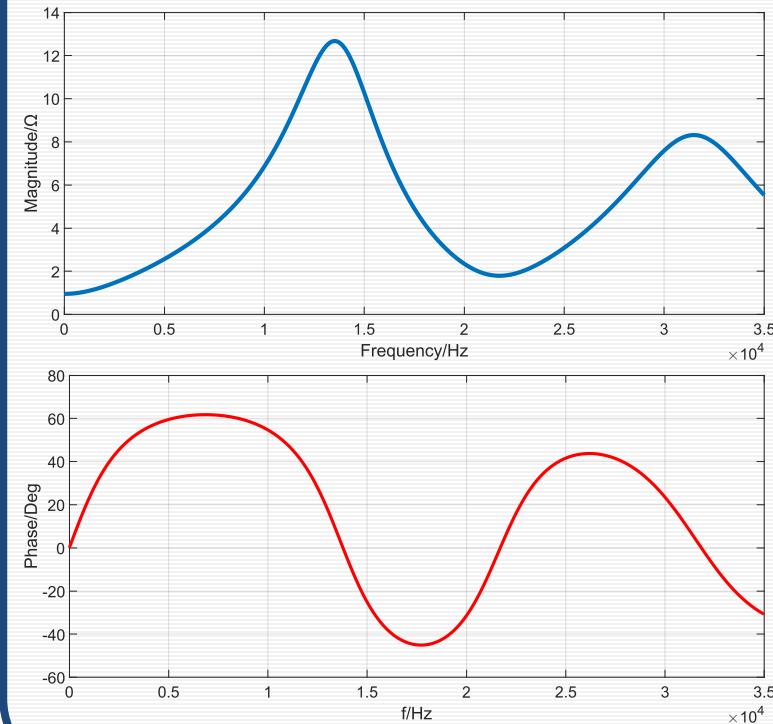


# PHiL Usecase: Impedance Replication of AIDAcosma

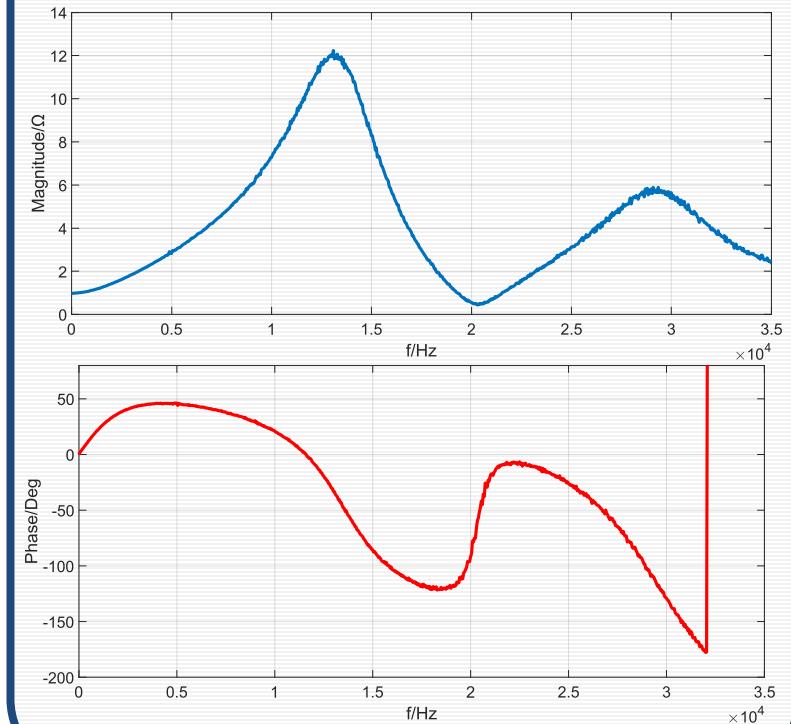
ONIS measurement  
on AIDAcosma



Simulink measurement of  
equivalent circuit on OP5707XG

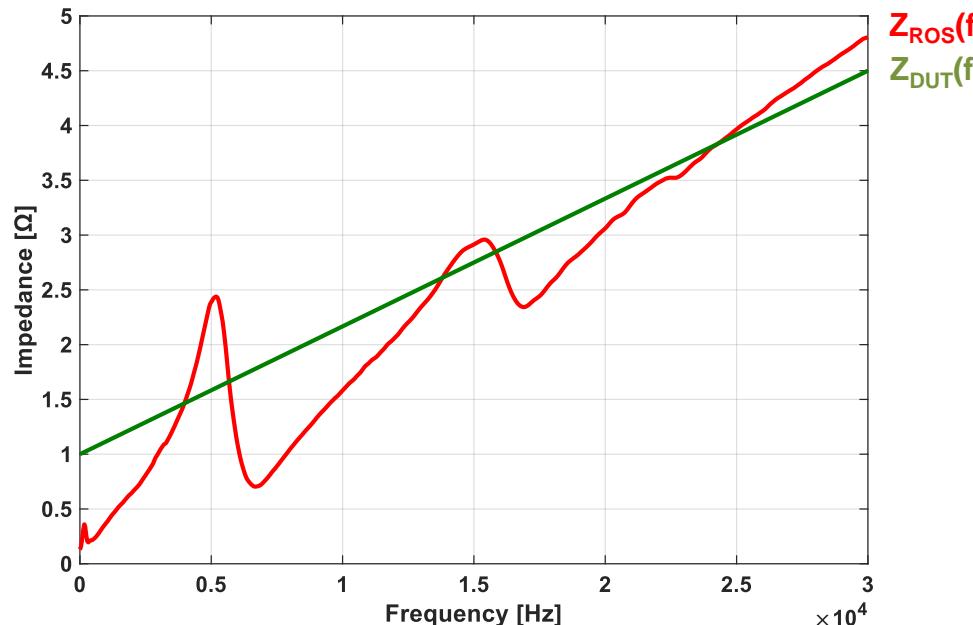


PHiL measurement  
with ONIS on Spitzenberger

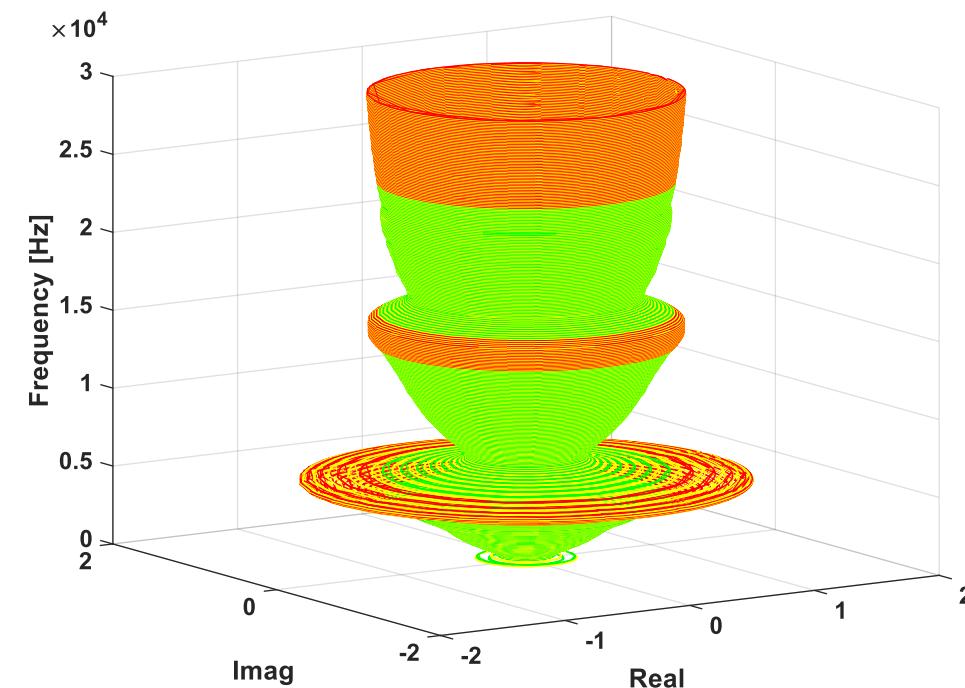


# Importance of Impedance Measurement in the Future

Exemplaric impedance of DUT and ROS in PHiL



Visualization of unstable frequency regions of PHiL

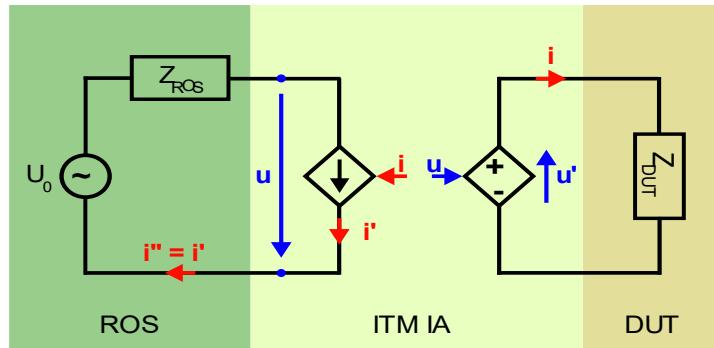


- ❖ PHiL gets unstable for  $Z_{ROS}(f) > Z_{DUT}(f)$  due to delays (Nyquist) → Interface Algorithm (IA) for compensation
- ❖ Online impedance measurement of ROS and DUT with OP5707XG and Spitzenberger
  - ✓ Current state: Online impedance measurement from 100 Hz – 30000 Hz in 0.3 s (realtime capable)
  - ✓ Implementation of a custom interface algorithm which allows for full-bandwidth PHiL simulation



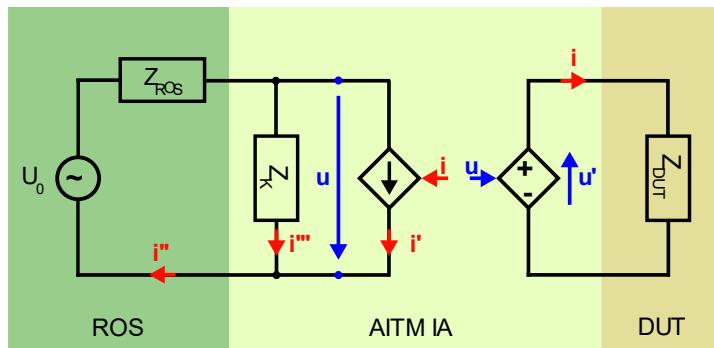
Thank you for participating!

# Stability criterion for PHiL – Interface Algorithms (IA)



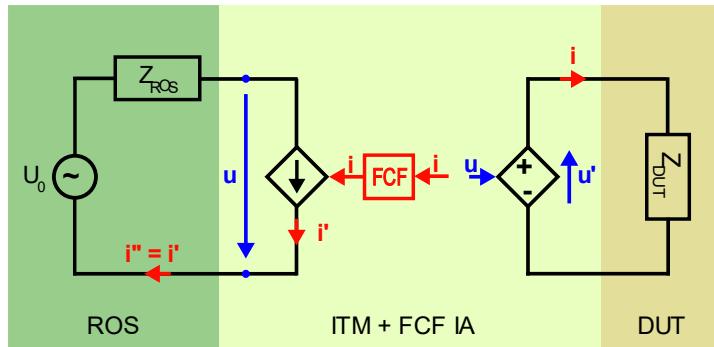
## ◆ Ideal Transformer Method (ITM)

- Direct coupling of  $u$  from simulation to hardware
- Direct coupling of  $i$  from hardware to simulation



## ◆ Advanced Ideal Transformer Method (AITM)

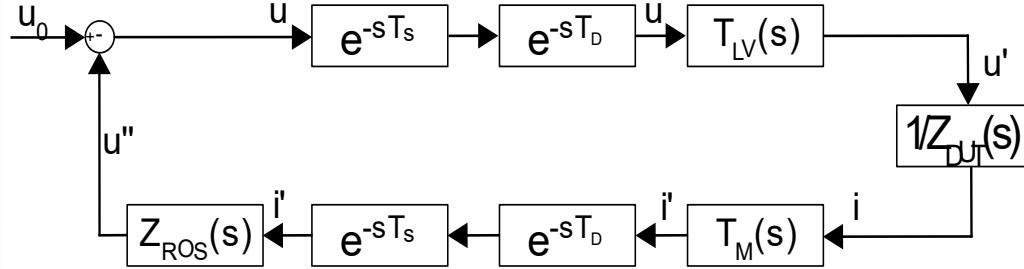
- Direct coupling of  $u$  from simulation to hardware
- Direct coupling of  $i$  from hardware to simulation
- Additional stabilization impedance



## ◆ Ideal Transformer Method (ITM) with Feedback Current Filter (FCF)

- Direct coupling of  $u$  from simulation to hardware
- Filtered signal  $i$  from hardware to simulation

# Stability criterion for PHiL – ITM theory

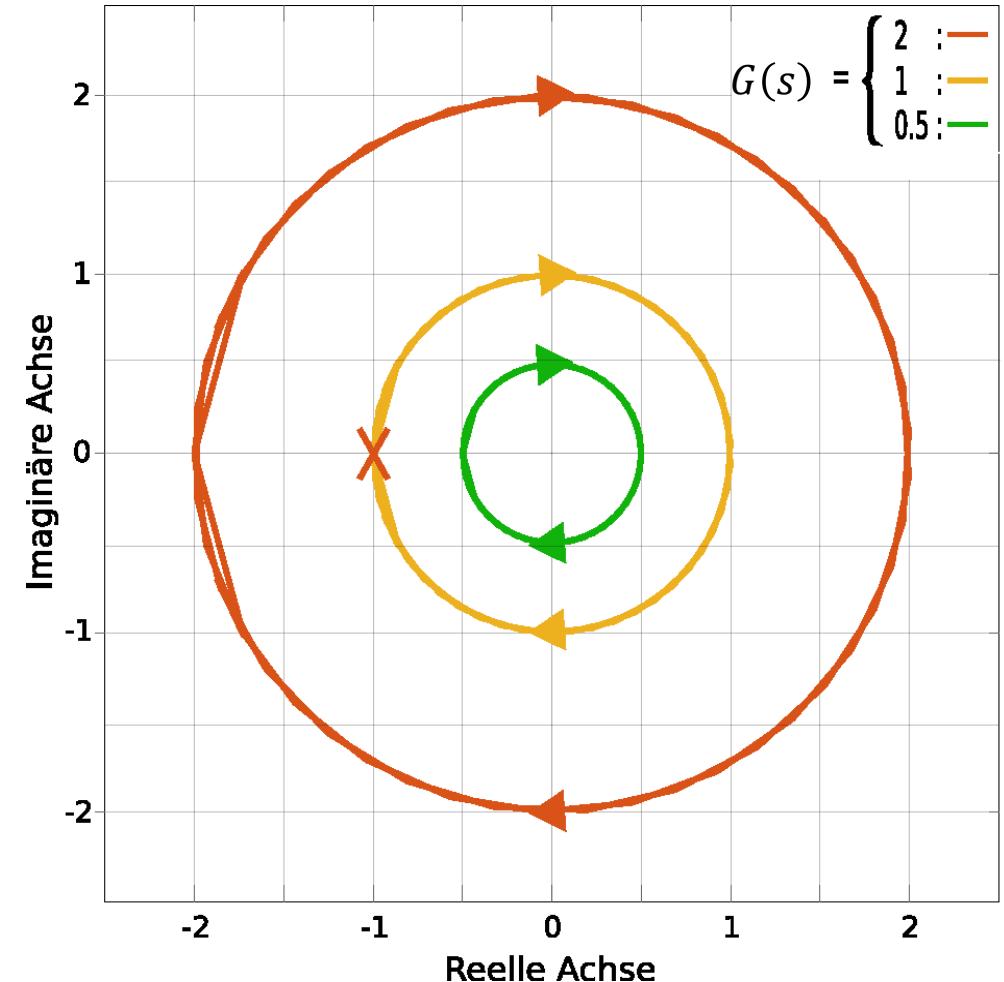


Open-loop is stable as  $T_{LV}(s)$  is always stable  
 Closed-loop stability:

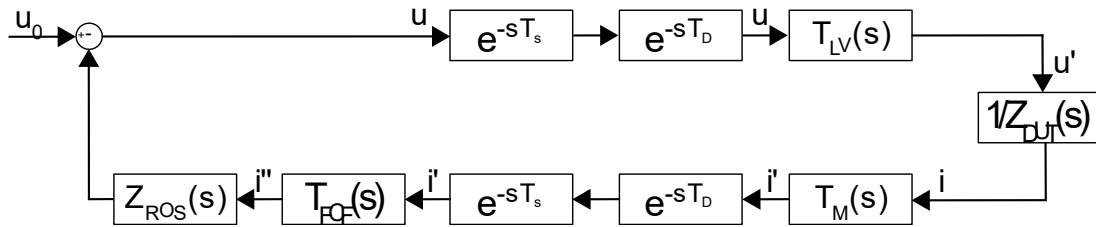
$$\rightarrow G(s) = e^{-sT_G} \cdot T_{LV}(s) \cdot T_M(s) \cdot \frac{Z_{ROS}(s)}{Z_{DUT}(s)}$$

$$\rightarrow G(s) \approx \frac{Z_{ROS}(s)}{Z_{DUT}(s)} \stackrel{!}{\leq} 1$$

$$\rightarrow Z_{DUT}(s) \geq Z_{ROS}(s)$$



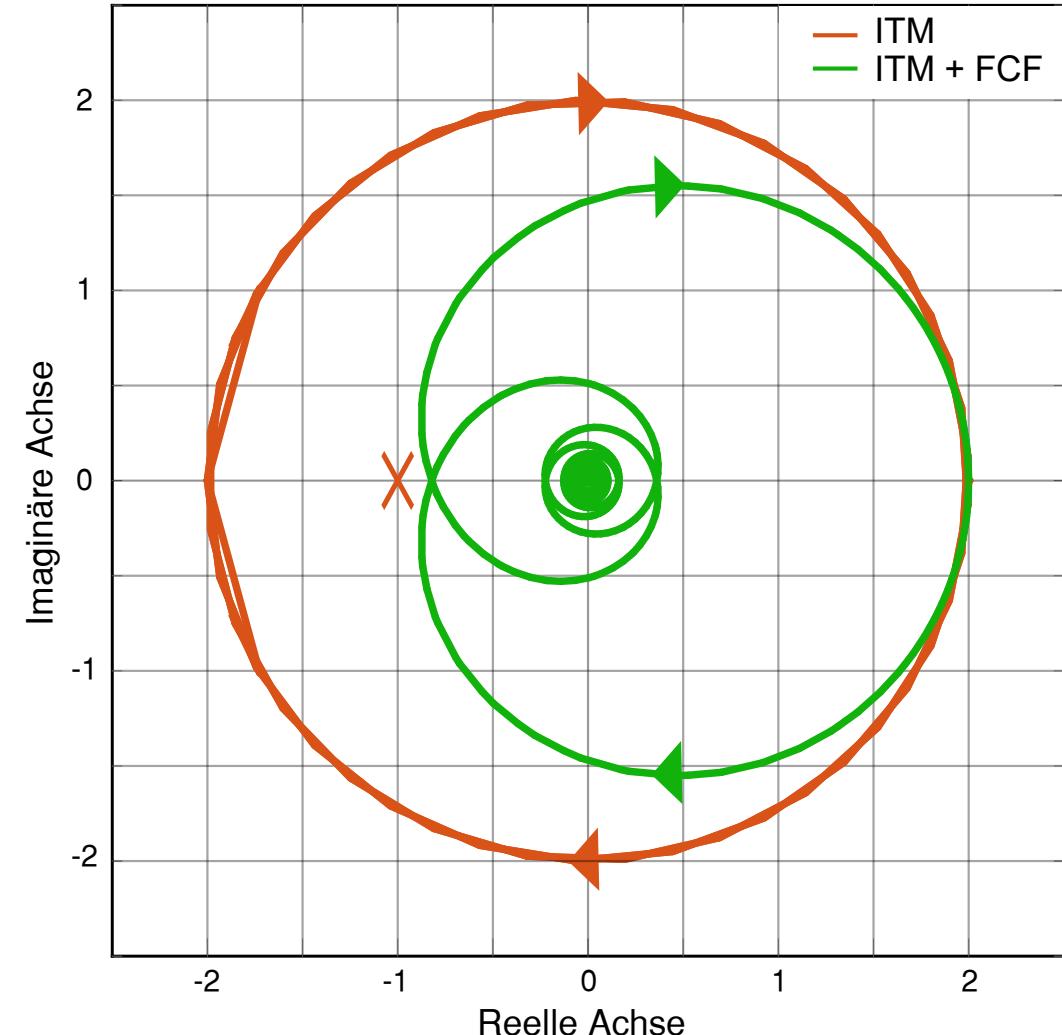
# Stability criterion for PHiL – ITM theory



$$G(s) = e^{-sT_G} \cdot T_{LV}(s) \cdot T_M(s) \cdot T_{FCF}(s) \cdot \frac{Z_{ROS}(s)}{Z_{DUT}(s)}$$

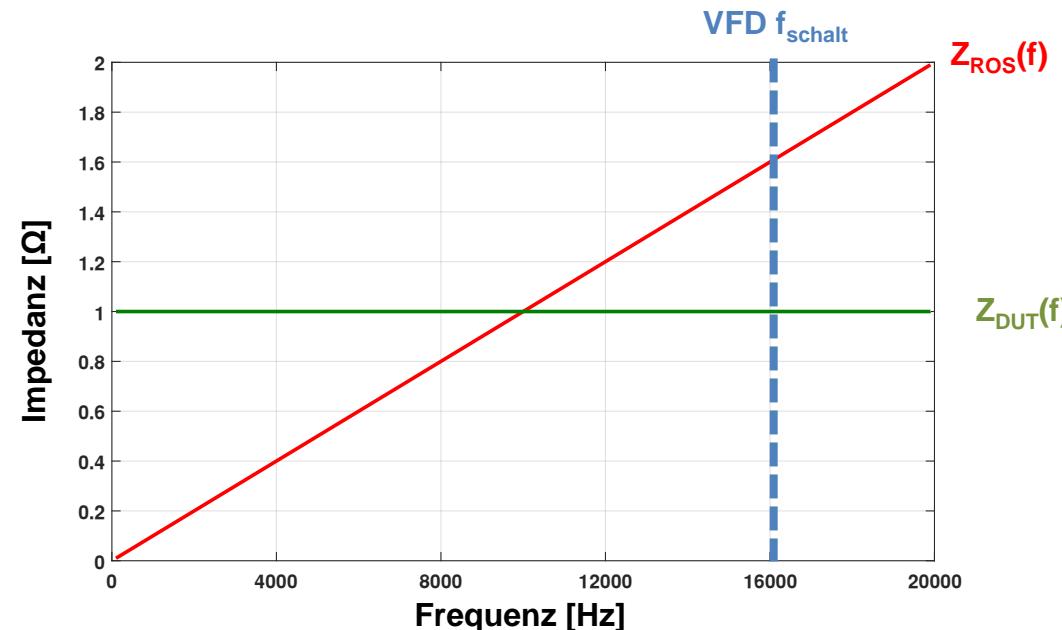
$$\rightarrow G(s) = T_{FCF}(s) \cdot \frac{Z_{ROS}(s)}{Z_{DUT}(s)} \stackrel{!}{\leq} 1$$

$\rightarrow$  choose matching  $T_{FCF}(s)$  to  $\frac{Z_{ROS}(s)}{Z_{DUT}(s)}$  and  $T_G$

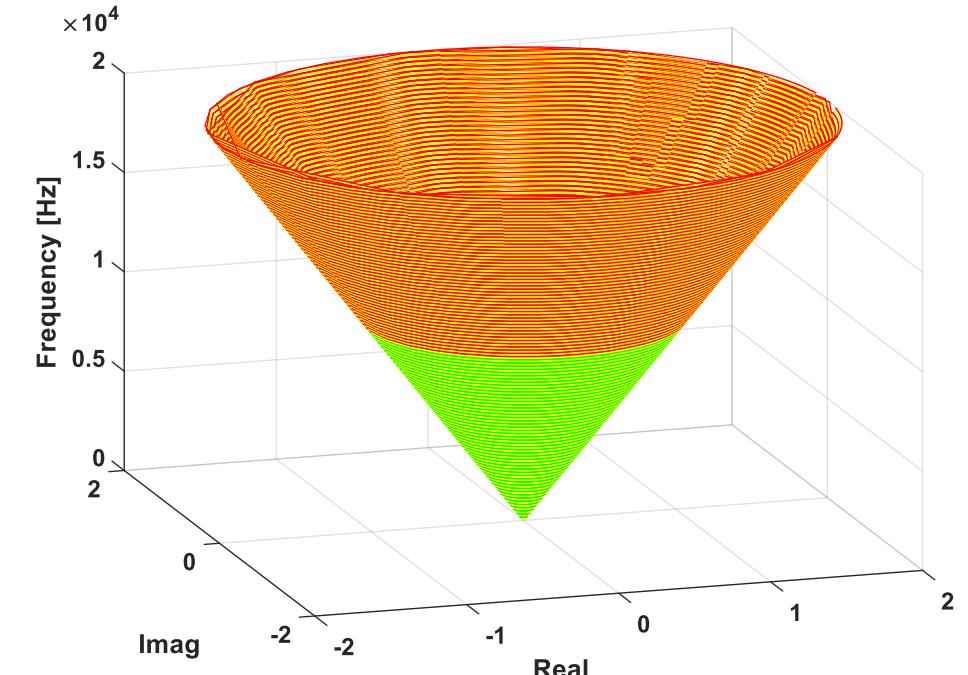


# Stabilitätskriterium für PHiL – ITM Stabilitätsbereich

Exemplarische frequenzabhängige Impedanzen bei PHiL



Stabilitätsbereiche für frequenzabhängige Impedanzen bei PHiL

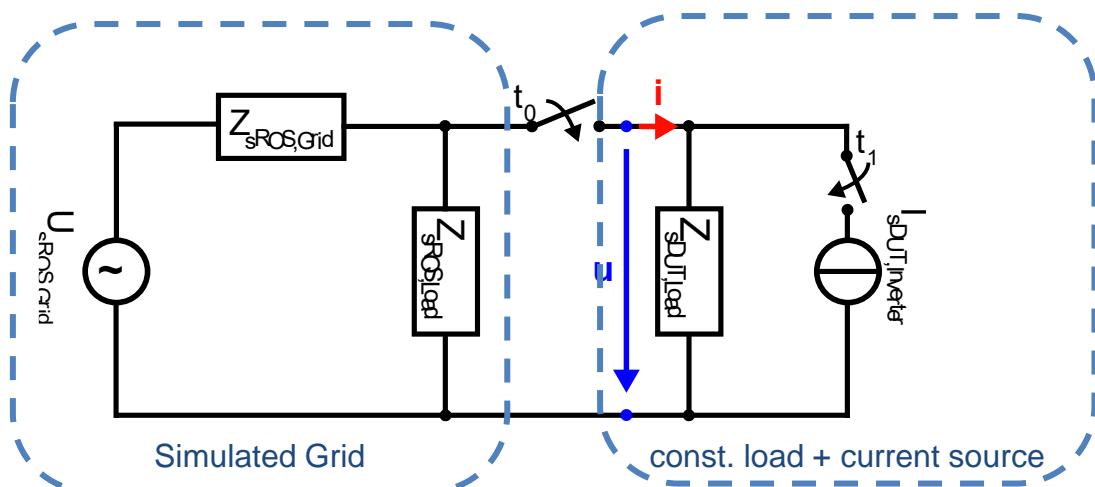


- ❖ Berücksichtigung frequenzabhängiger Impedanzen  
 $\{Z_{DUT}(f), Z_{ROS}(f)\} : f = [0; 20] \text{ kHz}$
- ❖ Anregung von Frequenzen aufgrund der Vielzahl schaltender Elemente im Netz (VFD, DC/DC,...)

# Stability criterion for PHiL - Examples

## Simulated grid expansion with constant load and variable current source

- ❖  $Z_{sROS,Load} = Z_{sDUT,Load} = 31,36 \Omega$  (marginally stable)
- ❖ constantly increasing current  $I_{sDUT,Inverter}$  from battery inverter starting from  $t = t_1$
- ❖  $Z_{sDUT} < Z_{sROS}$  @  $t = t_1$

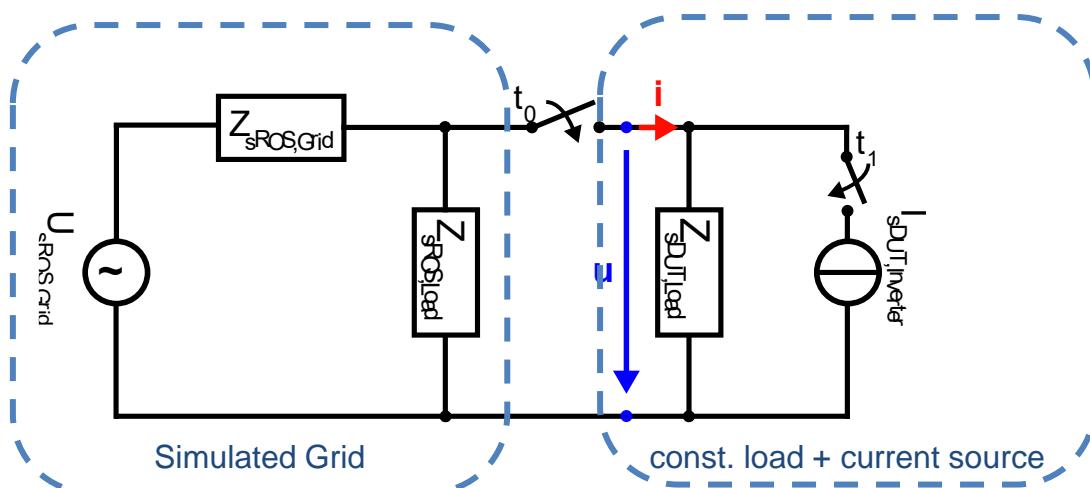
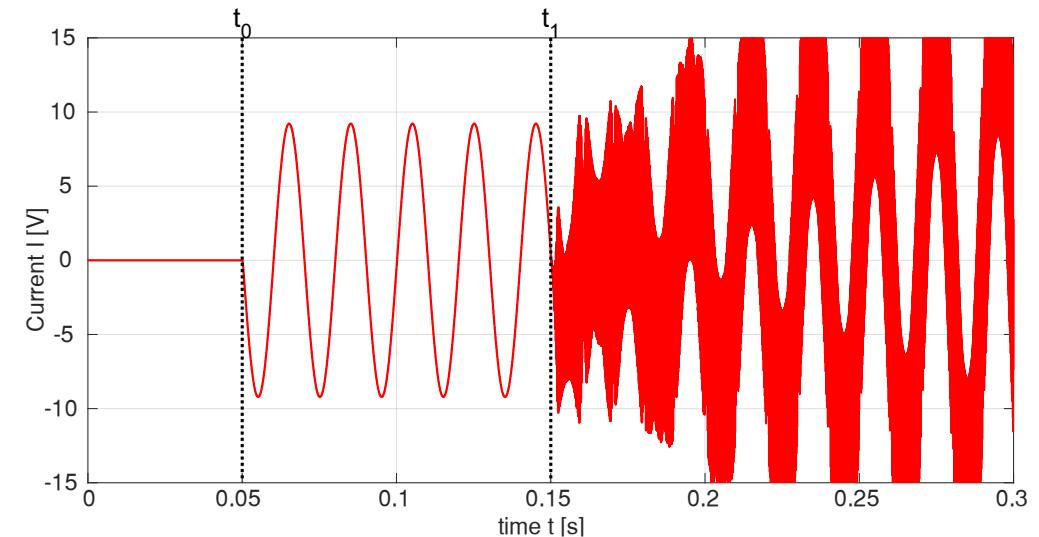


# Stability criterion for PHiL - Examples

## Simulated grid expansion with constant load and variable current source

- ❖  $Z_{sROS,Load} = Z_{sDUT,Load} = 31,36 \Omega$  (marginally stable)
- ❖ constantly increasing current  $I_{sDUT,Inverter}$  from battery inverter starting from  $t = t_1$
- ❖  $Z_{sDUT} < Z_{sROS}$  @  $t = t_1 \rightarrow$  instability with ITM

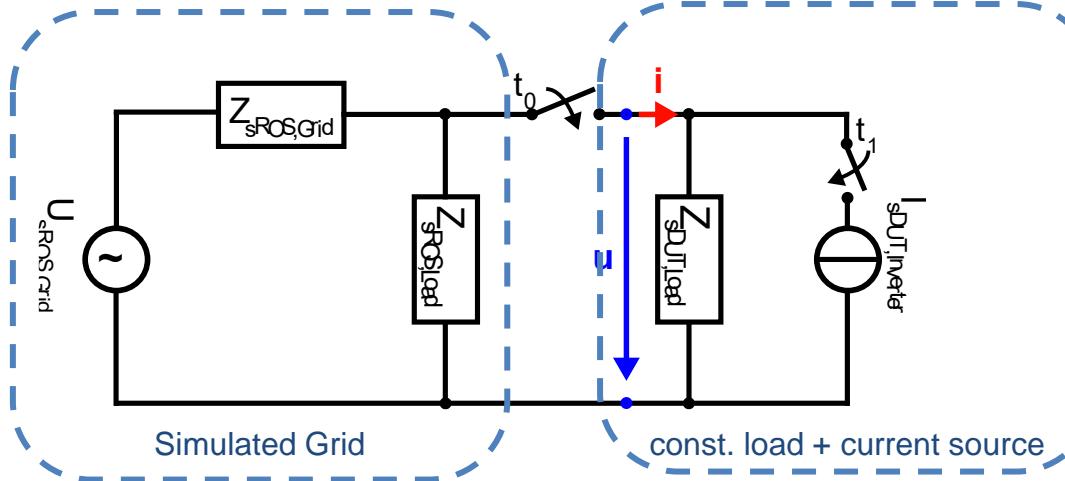
ITM



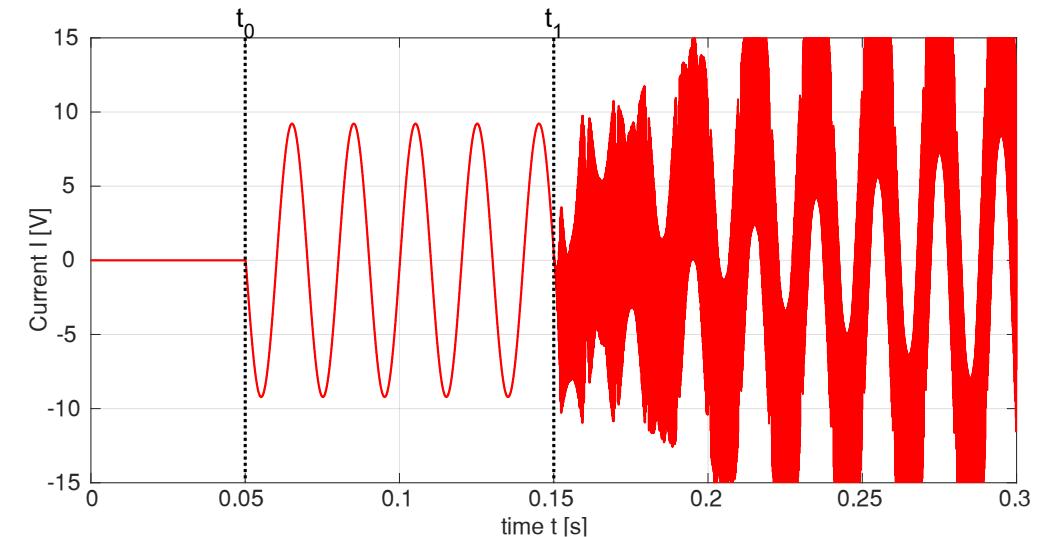
# Stability criterion for PHiL - Examples

## Simulated grid expansion with constant load and variable current source

- ❖  $Z_{sROS,Load} = Z_{sDUT,Load} = 31,36 \Omega$  (marginally stable)
- ❖ constantly increasing current  $I_{sDUT,Inverter}$  from battery inverter starting from  $t = t_1$
- ❖  $Z_{sDUT} < Z_{sROS}$  @  $t = t_1 \rightarrow$  instability with ITM  
→ stable with ITM + FCF



ITM



ITM  
+  
FCF

